# ALGORITHM FOR TRANSFORMATION OF WIND ROSE BY INCREASING OR DECREASING OF COMPASS DIRECTIONS

I. Butchvarov<sup>1</sup>, N. Gromkova<sup>2</sup>

Geophysical Institute, Bulgarian Academy of Sciences, 1113 Sofia, Acad. G. Bonchev Str., block 3, Bulgaria – www.geophys.bas.bg

<sup>1</sup>Section of Geomagnetism and Gravimetry – buch@geophys.bas.bg

<sup>2</sup> Section of Atmospheric Physics – gromkova@geophys.bas.bg

**Abstract.** The necessity to transform the standard (for Bulgaria) climatic 8-point wind roses, named *Observed Wind Roses* (OWR), was described in previous paper of the authors - Gromkova at al. The algorithm of calculation of the so-called *Primitive Wind Rose* (PWR) and further on the *Transformed Wind Rose* (TWR) in different number of compass directions then 8 is the purpose of the present paper.

Keywords: air pollution, wind rose.

#### Abbreviations:

PWR – Primitive Wind Rose
c.d.f cumulative distribution function
p.d.f. – probability density function

#### Introduction

The standard wind roses are represented with 8-compass directions – one for each 45° of the horizon, in the Climatic reference book of Bulgaria (1982). It was shown in a previous paper (Gromkova et al. 20 ..) that using a standard wind rose the determination of the annual mean air pollution concentration field from a point source is not adequate. For this reason the presented algorithm to transform the 8-point wind rose to a rose with more (or less, if it necessary) compass direction was created.

In Gromkova at al., 20... a wind direction was adopted as stochastic event and a random variable X with a corresponding *cumulative distribution function* – F(x) and a *probability density function* –  $p(x,\theta)$  was associated to it. In the present paper an algorithm for obtaining the *probability density function* –  $p(x,\theta)$  (p.d.f.) of the so-called *Observed Wind Roses* (OWR) – the rose from the Climatic reference book of Bulgaria (1982), and then to calculate the so-called *Transformed Wind Rose* in different compass directions (usually more) is presented.

### Determination of the parameter $\theta$ of the function $p(x, \theta)$

#### Variant 1

The function  $p(x,\theta)$  – probability density function – in this variant has the form:

$$p(x,a_i,b_i) = a_i + b_i x \tag{1}$$

in the intervals  $(x_i, x_{i+1}]$ . Between every two compass directions there is only one straight line. There are 2*n* unknowns:  $a_i$  – the *y*-intercept, and  $b_i$  – the slope of the line, if the compass directions are *n*. A method for determining the unknowns is given below:

Replacing  $N(x_i)$  and  $N(x_1)$  in the integrals of formulas (1) and (2) in Gromkova at al, 20..., by the empirical estimates  $\hat{N}_i$  and  $\hat{N}_1$ , and substituting  $x_i$  by  $x_i = 2(i-1)t$  in the limits of the integrals, the following expressions are obtained:

$$\hat{N}_{i} = \int_{(2i-3)t}^{2(i-1)t} (a_{i-1} + b_{i-1}z) dz + \int_{2(i-1)t}^{(2i-1)t} (a_{i} + b_{i}z) dz, \quad i = 2, 3, ..., n,$$
$$\hat{N}_{1} = \int_{(2n-1)t}^{2nt} (a_{n} + b_{n}z) dz + \int_{0}^{t} (a_{1} + b_{1}z) dz \quad i = 1 \quad (x_{1} = 0).$$

After integration and some transformations the following relations are reached:

$$M_i = d_{i-1} + d_i + (4i - 5)b_{i-1} + (4i - 3)b_i, \quad i = 2, 3, \dots, n,$$
(2)

$$M_1 = d_n + d_1 + (4n - 1)b_n + b_1, \quad i = 1,$$
(3)

where  $M_i = 2 \hat{N}_i / t^2$  and  $d_i = 2a_i / t$ .

The condition the strength lines defined with (1) to have equal values on both sides of the compass direction points (Gromkova et al, 20....) is:

$$d_i + 4(i-1)b_i = d_{i-1} + 4(i-1)b_{i-1}, \quad i = 2, 3, \dots, n,$$
(4)

$$d_1 = 4nb_n + d_n, \quad i = 1.$$
 (5)

The equations (2), (3), (4) and (5) represent a system of 2n linear equations in 2n unknowns. The solution of the system in brief follows:

The differences  $M_{i+1} - M_i$  and the sums  $d_{i+1} + d_i$  are made:

$$M_{i+1} - M_i = d_{i+1} - d_{i-1} - (4i - 5)b_{i-1} + 2b_i + (4i + 1)b_{i+1}, \ i = 2, 3, \dots, n - 1, (6)$$
  
$$M_2 - M_1 = d_2 - d_n - (4n - 1)b_n + 2b_1 + 5b_2, \ i = 1,$$
(7)

$$d_{i+1} - d_{i-1} = 4(i-1)b_{i-1} + 4b_i - 4ib_{i+1}, \quad i = 2, 3, \dots, n-1,$$
(8)

$$d_2 - d_n = 4b_n + 4b_1 - 4b_{i+1}, \quad i = 1.$$
(9)

The differences from (6) and (7) are replaced in the differences (8) and (9). A system of (n - 1) equations in *n* unknowns in respect of  $b_i$  is obtained:

$$M_{i+1} - M_i = b_{i-1} + 6b_i + b_{i+1}, \quad i = 2, 3, \dots, n-1,$$
(10)

$$M_2 - M_1 = b_n + 6b_1 + b_2, \quad i = 1.$$
(11)

Summarizing the equations (4) and (5) for i from 1 to n, the following expression is reached:

$$\sum_{i=1}^n b_i = 0.$$

Adding the last equality to (10) and (11) a system of n equations in n unknowns in respect of  $b_i$  is obtained.

The system is presented in a matrix form as A.B = F, where F is a column-vector with components  $f_i = M_{i+1} - M_i$ , for i = 1, 2, ..., n - 1, and  $f_n = 0$ , B is a column-vector with components the unknowns  $b_i$ , and A is a quadratic matrix of order n of the system coefficients. The system can be written as follows too:

$$\begin{pmatrix} u & 1 & 0 & 0 & \cdots & 0 & 0 & 0 & 1 \\ 1 & u & 1 & 0 & \cdots & 0 & 0 & 0 & 0 \\ 0 & 1 & u & 1 & \cdots & 0 & 0 & 0 & 0 \\ \cdots & \cdots \\ 0 & 0 & 0 & 0 & \cdots & 1 & u & 1 & 0 \\ 0 & 0 & 0 & 0 & \cdots & 0 & 1 & u & 1 \\ 1 & 1 & 1 & 1 & \cdots & 1 & 1 & 1 & 1 \end{pmatrix} \times \begin{pmatrix} b_1 \\ b_2 \\ b_3 \\ \cdots \\ b_{n-2} \\ b_{n-1} \\ b_n \end{pmatrix} = \begin{pmatrix} f_1 \\ f_2 \\ f_3 \\ \cdots \\ f_{n-2} \\ f_{n-1} \\ 0 \end{pmatrix} .$$

The diagonal elements, marked with u, are equal to 6. For obtaining the inverse matrix  $A^{-1}$  the matrix A is divided in 4 blocks:

$$\boldsymbol{A} = \begin{pmatrix} \boldsymbol{\alpha}_{11} \ \boldsymbol{\alpha}_{12} \\ \boldsymbol{\alpha}_{21} \ \boldsymbol{\alpha}_{22} \end{pmatrix},$$

where  $\alpha_{11}$  is a quasidiagonal matrix (Jacobian) of order n - 1 with main diagonal elements equal to 6 and with adjacent off-diagonal elements equal to 1,  $\alpha_{12}$  is a column-vector with components  $(\alpha_{12})_1 = 1$  and  $(\alpha_{12})_{n-1} = 1$ , and remaining elements equal to 0,  $\alpha_{21}$  is a rowvector with components equal to 1, and  $\alpha_{22}$  is a scalar equal to 1, too.

The inverse matrix is represented in blocks, too (Demidovitch and Maron, 1960):

$$\boldsymbol{A}^{-1} = \begin{pmatrix} \boldsymbol{\beta}_{11} \ \boldsymbol{\beta}_{12} \\ \boldsymbol{\beta}_{21} \ \boldsymbol{\beta}_{22} \end{pmatrix}$$

where:

$$\beta_{11} = \alpha_{11}^{-1} - \beta_{12} \alpha_{21} \alpha_{11}^{-1}, \qquad (12)$$

$$\beta_{12} = \alpha_{11}^{-1} \alpha_{12} (\alpha_{22} - \alpha_{21} \alpha_{11}^{-1} \alpha_{12})^{-1}, \qquad (13)$$

$$\beta_{21} = -\beta_{22}\alpha_{21}\alpha_{11}^{-1}, \tag{14}$$

$$\beta_{22} = (\alpha_{22} - \alpha_{21}\alpha_{11}^{-1}\alpha_{12})^{-1}.$$
(15)

In the expressions above  $\alpha_{11}^{-1}$  is the inverse matrix of  $\alpha_{11}$ . As the matrix  $\alpha_{11}$  is symmetrical, the inverse matrix  $\alpha_{11}^{-1}$  is symmetrical, too. Let's denote the elements of  $\alpha_{11}^{-1}$  by  $c_{ij}$  (*i*, *j* = 1, 2, ..., *n* - 1). It is possible to prove (see Appendix), that the analytical expression of  $c_{ij}$  is represented by the formula:

$$c_{ij} = -\frac{(Q^i - P^i)(Q^{n-j} - P^{n-j})}{(Q - P)(Q^n - P^n)}, \quad i \le j \le n - 1,$$
(16)

where

$$P = (\sqrt{u^2 - 4} - u)/2$$
 and  $Q = -(\sqrt{u^2 - 4} + u)/2$ 

Using the formula for  $c_{ij}$  it can be demonstrated that the elements of the matrices (blocks)  $-(\beta_{11})_{ij}, (\beta_{12})_i, (\beta_{21})_j$  and  $(\beta_{22})$  have the form:

$$\begin{split} (\beta_{11})_{ij} &= \frac{Q(Q^{j}-1)(Q^{i-j}-Q^{n-i})}{(Q^{2}-1)(Q^{n}-1)} , \quad j < i \le n-1 \\ (\beta_{11})_{ij} &= \frac{Q(Q^{n-j}-1)(Q^{j-i}-Q^{i})}{(Q^{2}-1)(Q^{n}-1)} , \quad i \le j \le n-1 \\ (\beta_{12})_{i} &= \frac{(Q-1)(Q^{n-i}+Q^{i})}{(Q+1)(Q^{n}-1)} , \qquad i \le n-1, \\ (\beta_{21})_{j} &= \frac{Q(Q^{n-j}-1)(Q^{j}-1)}{(Q^{2}-1)(Q^{n}-1)} , \qquad j \le n-1, \\ (\beta_{22}) &= \frac{(Q-1)(Q^{n}+1)}{(Q+1)(Q^{n}-1)} . \end{split}$$

The elements of the inverse matrix  $A^{-1}$  can be determined by using the formulas of the blocks  $\beta_{11}$ ,  $\beta_{12}$ ,  $\beta_{21}$  and  $\beta_{22}$  – the expressions (12), (13), (14) and (15). Finally, after the multiplication  $B = F A^{-1}$  the strength line coefficients  $b_i$  are determined according to the next expression:

$$b_{i} = \frac{Q}{(Q^{2} - 1)(Q^{n} - 1)} \times \left[\sum_{j=1}^{i-1} (Q^{j} - 1)(Q^{i-j} - Q^{n-i})f_{j} + \sum_{j=i}^{n} (Q^{n-j} - 1)(Q^{j-i} - Q^{i})f_{j}\right], \quad i = 1, ..., n.$$

To obtain the unknown  $d_i$  (respectively  $a_i$ ),  $d_n$  is defined by the expression (5), then it is substituted in (3) and  $d_1$  is represented by:

$$d_1 = (M_1 + b_n - b_1) / 2.$$

The remaining unknowns  $d_i$  for i = 2, ..., n are defined recursively by the formula (8):

$$d_i = d_{i-1} + 4(i-1)(b_{i-1} - b_i).$$

The coefficients  $a_i$  are obtained by the following expression:

$$a_i = t d_i / 2.$$

#### Variant 2

The analytical expression of the function p(x, a) in this case has the form:

$$p(x,a_i)=a_i,$$

defined in the intervals  $(x_i - t, x_i + t]$ , for i = 2, 3, ..., n, and in the intervals (360 - t, 360] and (0,t] for i = 1, i.e. for  $x_1 = 0$ . The unknowns are *n* for *n* directions.

The determination of these constants is as follows:

$$a_i = \hat{N}_i / 2t \, .$$

## Appendix

Let  $c_{ij}$  are the elements of the inverse matrix  $\alpha_{11}^{-1}$ . Then the following matrix equality is satisfied:

$(c_{11})$	$c_{12}$	$c_{13}$	•••	$C_{1,n-3}$	$C_{1,n-2}$	$c_{1,n-1}$		( u	1	0	•••	0	0	0)	
c21	$c_{22}$	<i>c</i> <sub>23</sub>		$C_{2,n-3}$	$C_{2,n-2}$	$C_{2,n-1}$		1	и	1		0	0	0	
c <sub>31</sub>	$c_{12} \\ c_{22} \\ c_{32} \\ \dots$	<i>c</i> <sub>33</sub>		$C_{3,n-3}$	$C_{3,n-2}$	$C_{3,n-1}$		0	1	и		0	0	0	
				•••			×			•••		•••			=E'
<i>C</i> <sub><i>n</i>-3</sub>	$c_{n-3,2}$ $c_{n-2,2}$ $c_{n-1,2}$	$C_{n-3,3}$		$C_{n-3,n-3}$	$C_{n-3,n-2}$	$C_{n-3,n-1}$		0	0	0		и	1	0	
$C_{n-2}$	$c_{n-2,2}$	$C_{n-2,3}$		$C_{n-2,n-3}$	$C_{n-2,n-2}$	$C_{n-2,n-1}$		0	0	0		1	и	1	
$C_{n-1}$	$_{,1}$ $c_{n-1,2}$	$C_{n-1,3}$		$C_{n-1,n-3}$	$C_{n-1,n-2}$	$C_{n-1,n-1}$	)	0	0	0		0	1	u )	

where *E* is the unit matrix. After multiplication of the *i*-th row of  $\alpha_{11}^{-1}$  by all columns of  $\alpha_{11}$ , the following equations are obtained:

$$uc_{i1} + c_{i2} = 0,$$
  

$$c_{i1} + uc_{i2} + c_{i3} = 0,$$
  
...  

$$c_{ii-1} + uc_{ii} + c_{i,i+1} = 1,$$
  

$$c_{ii} + uc_{i,i+1} + c_{i,i+2} = 0,$$
  
...  

$$c_{i,n-3} + uc_{i,n-2} + c_{i,n-1} = 0,$$
  

$$c_{i,n-3} + uc_{i,n-2} + c_{i,n-1} = 0,$$
  

$$c_{i,n-2} + uc_{i,n-1} = 0.$$
(18)

It is obvious that for  $i = 2, 3, ..., n-3, j > i, c_{ij}$  satisfies the recurrence relation:

$$c_{i,j-1} + uc_{ij} + c_{i,j+1} = 0. (19)$$

To obtain the common term of this recursion, its characteristic equation is used (Markushevitch, 1975):

$$q^2 + uq + q = 0.$$

The roots of this equation, denoted by P and Q, are:

$$P = (\sqrt{u^2 - 4} - u)/2$$
 and  $Q = -(\sqrt{u^2 - 4} + u)/2$ .

They are real when  $u \ge 2$ , i.e. in the discussed case, because u = 6:  $Q = -(\sqrt{8} + 3) \approx -5.8284$ . The common term of the relation (19) is presented by the expression (Markushevitch, 1975):

$$c_{ij} = G_i P^{j-i} + H_i Q^{j-i}, \quad i = 2, 3, ..., \quad n-3, j > i.$$
 (20)

The coefficients  $G_i$  and  $H_i$  are different for each *i*, i.e. for every row.

The first two terms of the above expression – for j = i and j = i + 1 – have the form:

$$c_{ii} = G_i + H_i, \tag{21}$$

$$c_{i,i+1} = G_i P + H_i Q, \tag{22}$$

and the last two – for j = n-2 and j = n-1:

$$c_{i,n-2} = G_i P^{n-2-i} + H_i Q^{n-2-i},$$
(23)

$$c_{i,n-1} = G_i P^{n-1-i} + H_i Q^{n-1-i}.$$
(24)

To determine the unknown coefficients  $G_i$  and  $H_i$  the equalities (17), written in the form:

$$uc_{ii} + c_{i,i+1} = D_{ii-1}, (25)$$

and the expression (18), that are not terms of the recurrence relation (19), are used too.  $D_{i,i-1}$  in the above expression according (17) is  $D_{i,i-1} = 1 - c_{i,i-1}$ . As the matrix  $\alpha_{11}^{-1}$  is symmetric  $c_{i,i-1} = c_{i-1,i}$ . However the element  $c_{i-1,i}$  is determined from the recurrence relation by multiplication of the *i*-1-th row and therefore  $D_{i,i-1}$  is determined too.

It is known that u = -(P + Q) and PQ = 1 for the roots of the quadratic equation. Replacing (21) and (22) in (25), (23) and (24) in (18) and u in (25) and (18) and after some processing the following system of equations for  $G_i$  and  $H_i$  is obtained:

$$G_i Q + H_i P = -D_{i,i-1},$$
  
$$G_i P^{n-i} + H_i Q^{n-i} = 0.$$

The solution of the system in respect to  $G_i$  and  $H_i$  is:

$$G_i = -\frac{Q^{n-i}}{Q^{n+1-i} - P^{n+1-i}} D_{i,i-1},$$
(26)

$$H_{i} = \frac{P^{n-i}}{Q^{n+1-i} - P^{n+1-i}} D_{i,i-1}.$$
 (27)

Determining  $D_{i,i-1}$ , for i = 2, 3, ... and s.o., it can be shown that

$$D_{i,i-1} = \frac{(Q^{i} - P^{i})(Q^{n+1-i} - P^{n+1-i})}{(Q - P)(Q^{n} - P^{n})}.$$

After replacing  $D_{i,i-1}$  in (26) and (27) and then  $G_i$  and  $H_i$  in (26), the expression (16) in the main text – the formula for the coefficients  $c_{ij}$  – is reached.

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#### Алгоритъм за преобразуване на розата на вятъра чрез увеличаване или намаляване на румбовете

#### И. Бъчваров, Н. Громкова

Резюме.. Необходимостта да се преобразува стандартната за България климатична 8румбова роза на вятъра (наречена тук *Наблюдателна Роза на Вятъра* (НРВ)) възникна във връзка с определянето на концентрацията на климатичното (средногодишното) замърсяване на въздуха от точков източник, което е основна цел на оценките на въздействие върху околната среда (т.н. OBOC). В предната публикация (Gromkova at al.) бяха представени редица теоретични примери за преимуществата на разработения алгоритъм за трансформиране на розата на вятъра при получаване на полето на приземните концентрации, в сравнение с използването на 8-румбовата роза, дадена в климатичния справочник. Тук е представен математическия апарат, използуван за получаване на рози с различен брой румбове.